

# Optical directional coupler and Mach-Zehnder interferometer enhanced via 4H-SiC phonons

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## ABSTRACT

Surface phonon polaritons (SPhPs), similar to its cousin phenomenon surface plasmon polaritons (SPPs), are quasi-neutral particles resulting from light-matter coupling that can provide high modal confinement and long propagation in the mid to long infrared (IR). Mach-Zehnder interferometer (MZI) is a combination of two connected optical directional couplers (ODC). With the use of SPhPs, sub-wavelength feature sizes and modal areas can be achieved and to this end a hybrid SPhP waveguide, where propagation length and modal area can be trade-off, will be employed in the design of an ODC and MZI. This endeavor analyzes and characteristics both an ODC and MZI using commercially available numerical simulation software employing finite element method (FEM). The ODC and MZI are design using a novel SPhP hybrid waveguide design where a 4H-SiC substrate provides the polariton mode. The output ports power and relative phase difference between ports are investigated. SPhP enhanced ODC and MZI has applications including, but not limited to, next-generation ultra-compact photonic integrated circuits and waveguide based IR sensing.

**Keywords:** Surface Phonon Polaritons(SPhP), Mach-Zehnder Interferometer, 4HSilicon Carbide (SiC), Optical Directional Coupler (ODC), Couple Mode Theory (CMT)

## 1. INTRODUCTION

In recent years, a push for minimization of optical and photonic devices has led in advancement and maturing of waveguide technology that exploits ultra-confinement of surface plasmon polaritons (SPPs) in the optical to ultraviolet (UV) spectrum<sup>1,2</sup>. SPPs result from the coupling between the valence electrons in metals and electromagnetic radiations resulting in a transverse magnetic (TM) surface mode at the metal/dielectric interface. Similar in the case of surface phonon polariton (SPhP), a TM surface mode is present, but at a polar dielectric/dielectric interface. The underlying process results from the coupling of the lattice vibrations, phonons, in the polar dielectrics in a band of frequencies where the dielectric permittivity of the polar dielectric becomes negative known as the Reststrahlen band<sup>3,4</sup>. The mathematical treatment for the dispersion relationship for SPhP is similar to that of SPP, and is as follows<sup>1</sup>:

$$k_{SP} = k_0 \sqrt{\frac{\epsilon_m \epsilon_d}{\epsilon_m + \epsilon_d}}, \quad (1)$$

where  $\epsilon_m$  is for metal in the SPP or polar dielectric in SPhP case,  $\epsilon_d$  is the dielectric half space, and  $k_0$  is the free space wavenumber. The SPhP hybrid waveguide under consideration is shown in Figure 1 at an operating wavelength of 12.4  $\mu\text{m}$ <sup>1,5,6</sup>. The effective refractive index and propagation length can be determined from eq. 1 as the following:

$$n_{sp} = \text{Re} \left\{ \sqrt{\frac{\epsilon_m \epsilon_d}{\epsilon_m + \epsilon_d}} \right\}, \quad (2.a)$$

$$L_m = \frac{1}{2\text{Im}\{k_{SP}\}}. \quad (2.b)$$

With the use of coupled-mode theory (CMT)<sup>1,7-9</sup>, the hybrid mode can be described as a superposition of two uncoupled modes; a waveguide tracer mode and SPhP TM mode. Therefore, a modal character can be defined as:

$$|a|^2 = \frac{n_{hyb} - n_{SP}}{(n_{hyb} - n_{WG}) + (n_{hyb} - n_{SP})}, \quad (3)$$

where  $n_{sp}$  describes the pure TM polariton surface mode,  $n_{WG}$  is the waveguide tracer mode, and  $n_{hyb}$  is the resulting hybrid waveguide mode. Here mode character ranges from 0 to 1 where 0 is for pure TM surface mode and 1 is for waveguide tracer mode.

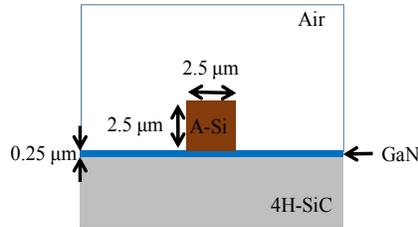


Figure 1. Design hybrid SPhP enhanced waveguide cross-section under consideration.

Surface polaritons can provide ultra-compacted modes when hybridized, and the modal area can be defined using energy density:

$$A_m = \frac{\iint W(\mathbf{r}) dx dy}{\max\{W(\mathbf{r})\}}, \quad (4)$$

where, in the case of uniaxial material, i.e. 4H-SiC<sup>10</sup>,

$$W(\mathbf{r}) = \frac{1}{2} \left[ \frac{d(\varepsilon_{\perp}(\omega)\omega)}{d\omega} |E_x|^2 + \frac{d(\varepsilon_{\parallel}(\omega)\omega)}{d\omega} |E_y|^2 + \frac{d(\varepsilon_{\perp}(\omega)\omega)}{d\omega} |E_z|^2 + \mu_0 |H(\mathbf{r})|^2 \right]. \quad (5)$$

Modal area is typically normalized to the diffraction-limited area in free space:  $A_0 = \lambda_0^2/4$ . Ansys high frequency structural simulator (HFSS) is a commercial finite element method (FEM) solver where driven HFSS models were employed to characterize the hybrid waveguide shown in Figure 1 and the optical directional coupler (ODC) and Mach-Zehnder interferometer (MZI) in the following sections. Table 1 tabulates the numerical results for effective hybrid index, propagation length, normalized modal area, and modal character for the hybrid waveguide employed in designing the ODC and MZI.

Table 1. The HFSS driven model analysis for the hybrid SPhP enhanced waveguide shown in Figure1.

$n_{hyb}$	$L_m$ [ $\mu\text{m}$ ]	$A_m/A_0$	$ a ^2$
1.62	49.0	1.57E-2	55.8%

This endeavor reports on first numerical results, to the best of the authors' knowledge, of optical directional coupler and Mach-Zehnder interferometer using a hybrid SPhP waveguide in the mid to long IR spectrum. ODC and MZI are elementary devices that can enable technology in applications like quantum information, photonic integrated circuits (PIC), and IR sensing technology<sup>11-15</sup>.

## 2. OPTICAL DIRECTIONAL COUPLER DESIGN

An ODC is a two-input-two-output optical device with isolated input and outputs ports. In the center is a coupling region that allows the transfer of power between the branches as a function of coupling length "L". Four s-bend waveguides formed out of the A-Si traces are used to create the ODC. To aid in design of the ODC, two lines were investigated for coupling and isolation from each other as shown in Figure 2. As it can be seen from Figure 2, under 3% of the power is coupled into the other line with separation "s" that is greater than 4  $\mu\text{m}$  therefore; to provide isolation of the input and output ports are separated by a distance greater than 4  $\mu\text{m}$  as can be seen in Figure 3.

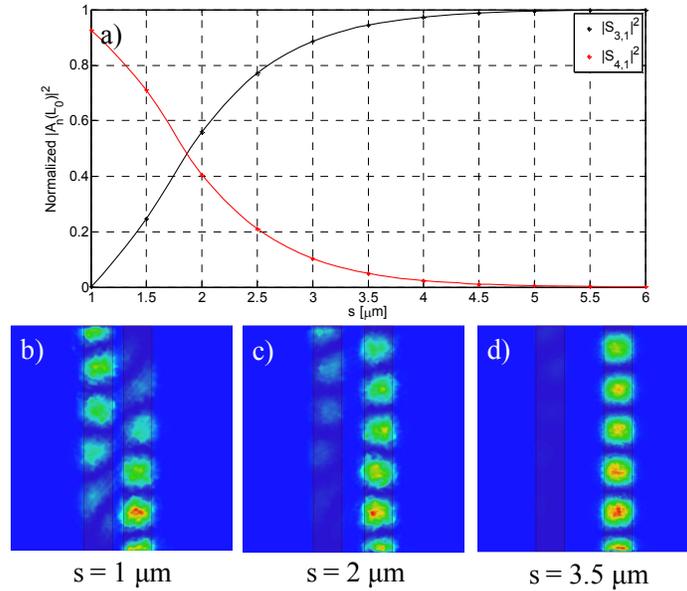


Figure 2. a) The normalized power for both output ports 3 and 4 as a function of waveguide separation “s” is shown. The  $|E|^2$  on the 4H-SiC/GaN interfaces is shown for s equal to 1  $\mu\text{m}$  (b), 2  $\mu\text{m}$  (c), and 3.5  $\mu\text{m}$  (d).

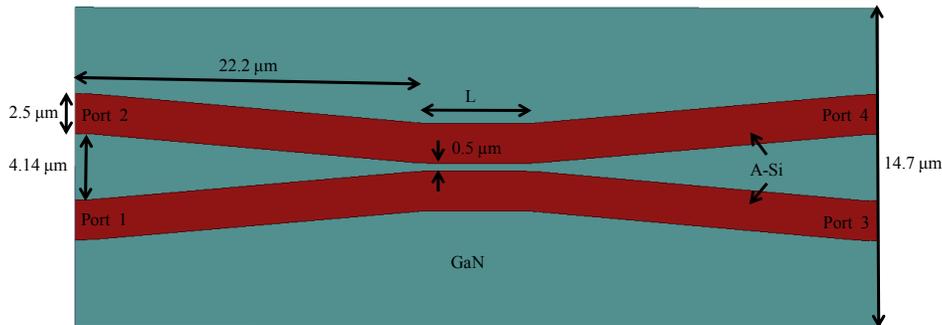


Figure 3. ODC top view under consideration with dimension labeled.

The output power for a phased matched or symmetrical ODC is governed by<sup>7,16</sup>:

$$|A_1(z)|^2 = e^{-2\alpha L} \cos^2\left(\frac{\pi}{2L_0} L\right), \quad (6.a)$$

$$|A_2(z)|^2 = e^{-2\alpha L} \sin^2\left(\frac{\pi}{2L_0} L\right), \quad (6.b)$$

where  $L_0$  is the transfer length (or  $2L_0$  is called the beat length) and  $\alpha$  is the field attenuation due to propagation losses. The transfer length is the coupling length needed to couple the output power from one waveguide into another. Figure 4.a show the sinusoidal dependence of port output power with coupling distance as determined by eq. 6. For this particular design the transfer length is 14.1  $\mu\text{m}$  which can be seen in Figure 4.a. The phase difference between the output ports can be seen in part b of Figure 4. Given that ellipsometry-measured material properties<sup>17</sup> are imported into HFSS, the variation off of the  $\pm 90^\circ$  in the phase difference is a result of the lossy nature and internal damping of the materials in particular the polar dielectric, 4H-SiC, that is used. The  $|E|^2$  at the 4H-SiC/GaN interfaces at approximately 3dB splitter is shown in Figure 4.c. It can be seen from the  $|E|^2$  of the 3dB splitter in Figure 4.c, due to the gradual bend of the s-bend the transfer of the field from waveguide one into two occurs within the bend.

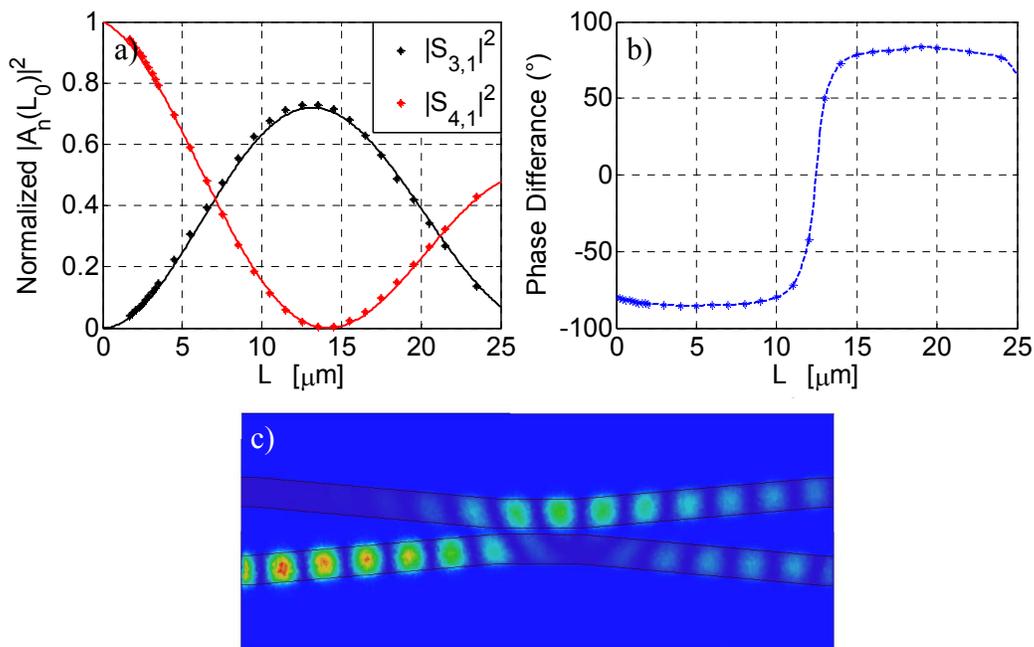


Figure 4. The normalized power a) and phase difference between the ports b) of the output ports at varies coupling lengths. c) The  $|E|^2$  at the 4H-SiC/GaN interfaces is shown for when the ODC is a 3dB splitter.

### 3. MACH-ZEHNDER INTERFEROMETER DESIGN

Next, a MZI is designed and characterized numerically using HFSS. Two ODCs are combined with a 5.0  $\mu\text{m}$  straight waveguide sections connecting the two ODC as seen in Figure 5. Similar as in the case of the ODC, the coupling region of the two ODCs were tuned simultaneously with the same length. The resulting normalized output power is shown in Figure 6.a as a function of coupling length. As before in the ODC case, an exponentially decaying sinusoidal fit was used as seen in Figure 6.a. Figure 6.b shows the  $|E|^2$  at the 4H-SiC/GaN interfaces for when the coupling length is at the 3dB splitter/combiner point.

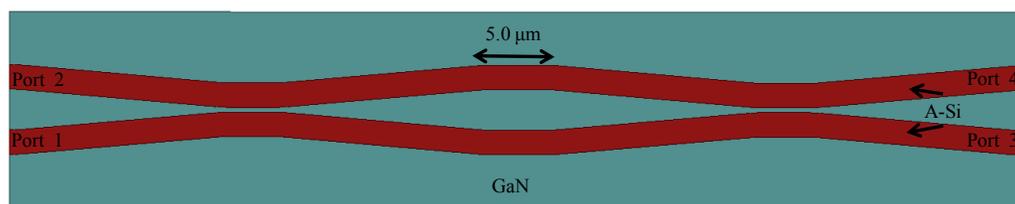


Figure 5. The top view of the MZI under consideration is shown.

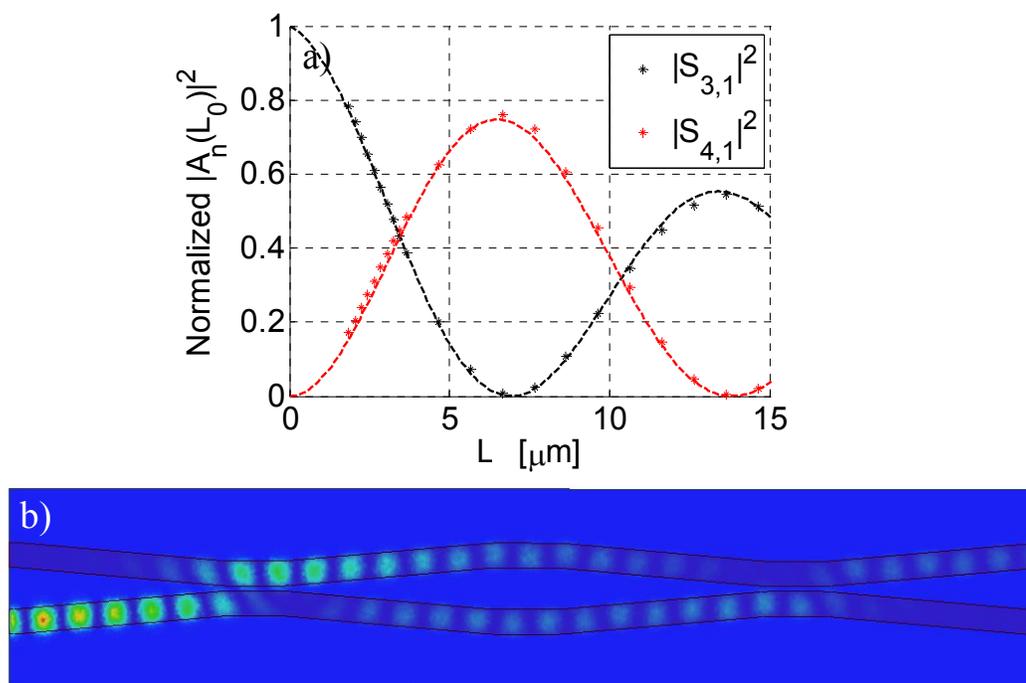


Figure 6. a) The normalized output port power is shown as a function of coupling length of the ODC. b) The  $|E|^2$  at the 4H-SiC/GaN interfaces is shown for when the ODC coupling length are at 3dB splitter/combiner.

#### 4. CONCLUSION

In conclusion, a hybrid SPhP enhanced waveguide was implemented in the design of an ODC and MZI using FEM solver HFSS. Both devices, ODC and MZI, have a transverse size smaller than the free space wavelength of approximately  $9.25 \mu\text{m}$ . Due to nature of the surface polaritons, subwavelength or ultra-compactness transverse size ODC and/or MZI are potentially achievable by decreasing the modal area of the initial hybrid waveguide however; at a cost of the propagation length<sup>1,5</sup>. With the MZI device length on the order of  $100 \mu\text{m}$ , a reduction of propagation length would not be appealing given the propagation length tabulated in Table 1. Alternatively, a reduction of the transverse separation between the inputs could be traded-off for a reduction in isolation to reduce transverse size. Future work will include investigating using other hybrid waveguide design, in particular that use of equivocated polar dielectric metal-insulator-metal (MIM) or insulator-metal-insulator (IMI) heterostructure<sup>2</sup>. Also, the concept of hybrid materials where polar dielectrics couple with graphene<sup>18,19</sup> resulting in a material gains attributed of the un-joined material<sup>20-22</sup>. In particular, hybrid material retain graphene electrooptic properties<sup>20,21</sup> make it possible for ultra-compact optical switches and modulators in the mid to long IR with the used of surface polaritons<sup>19,23</sup>.

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